Australian Standard®

Conductors—Bare overhead, aluminium and aluminium alloy—Steel reinforced

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PREFACE

This Standard was prepared by the Standards Australia Committee on Overhead Lines to supersede all three parts of AS 1220, Aluminium conductors steel reinforced for overhead power transmission purposes:

Part 1: 1973 Galvanized steel reinforced (ACSR/GZ)
Part 2: 1973 Aluminized steel reinforced (ACSR/AZ)
Part 3: 1973 Aluminium-clad steel reinforced (ACSR/AC)

The Standard deals with composite conductors made with aluminium or aluminium alloy wires, reinforced with steel wires. Three types of steel wire are included as alternatives, i.e. zinc-coated (GZ), aluminium-coated (AZ) or aluminium-clad (AC).

In addition, the Standard provides for specific wire sizes in the range 1.60 mm to 4.75 mm, with a range of standard sizes of stranded construction conductors. Furthermore it provides for a range of new conductors containing steel and aluminium alloy wires which reflect actual usage of conductors throughout Australia.

This edition of the Standard differs from AS 1220-1973 as follows:

- (a) In determining conductor sizes, a range of wire sizes has been provided similar to the range of wires specified in the 1973 edition, but facility is also provided for conductors with other dimensions to be supplied by reference to this Standard.
- (b) To assist users in selecting the most suitable conductor for a particular application, the calculated equivalent aluminium area, conductor breaking load, and d.c. resistance for the standard conductors are given.
- (c) Section 2: Wire sizes have been rationalized.
- (d) Section 3: The number of standard sizes, especially in the alloy range has been reduced and preferred sizes are indicated.
- (e) Section 4: For test purposes, requirements have been added to sequentially identify wire and conductor during production.
- (f) Appendix B: Now includes the theoretical basis for the calculation of modulus of elasticity and coefficient of linear expansion.
- (g) Appendix E: The code name system has been changed to permit the identification of alloy conductors by reference to existing ACSR code names.
- (h) Appendix F: This new Appendix has been included which highlights items which should be specified by the purchaser or agreed between purchaser and manufacturer at the time of order.

In the preparation of this Standard, reference was made to the following Standards:

IEC 207 IEC 208 Aluminium stranded conductors Aluminium alloy stranded conductors (aluminiummagnesium-silicon) Aluminium alloy conductors, steel reinforced IEC 210 IEC 468 Method of measurement of resistivity of metallic materials Aluminium coated (aluminized) steel core wire for **ASTM B 341** aluminium conductors, steel reinforced ACSR/AZ Zinc-coated (galvanized) steel core wire for aluminium conductors, steel reinforced, ACSR (Metric) ASTM B 498M Aluminium-clad steel core wire for aluminium conductors, **ASTM B 502** aluminium-clad steel reinforced SS 424 08 13 Aluminium alloy wire for stranded conductors for overhead

Acknowledgement is made of the assistance received from those sources.

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STANDARDS AUSTRALIA

Australian Standard

Conductors—Bare overhead, aluminium and aluminium alloy—Steel reinforced

SECTION 1. SCOPE AND GENERAL

- 1.1 SCOPE. This Standard specifies requirements and tests for composite bare electrical conductors for overhead power transmission purposes, incorporating aluminium or aluminium alloy wires and steel wires in their construction.
- 1.2 NOMENCLATURE. Aluminium and aluminium alloy conductors steel reinforced covered by this Standard include the following types, with the code for each in parentheses:
- (a) Aluminium 1350, zinc-coated (galvanized) steel reinforced (ACSR/GZ)².
- (b) Aluminium 1350, aluminium-coated (aluminized) steel reinforced (ACSR/AZ)².
- (c) Aluminium 1350, aluminium-clad steel reinforced (ACSR/AC)².
- (d) Aluminium alloy 1120, zinc-coated (galvanized) steel reinforced (AACSR/GZ/1120).
- (e) Aluminium alloy 1120, aluminium-coated (aluminized) steel reinforced (AACSR/AZ/1120).
- (f) Aluminium alloy 1120, aluminium-clad steel reinforced (AACSR/AC/1120).
- (g) Aluminium alloy 6201A, zinc-coated (galvanized) steel reinforced (AACSR/GZ/6201)³.
- (h) Aluminium alloy 6201A, aluminium-coated (aluminized) steel reinforced (AACSR/AZ/6201)³.
- (i) Aluminium alloy 6201A, aluminium-clad steel reinforced (AACSR/AC/6201).

NOTES:

- A list of code names which may be used to refer to a specific type and construction of conductor is given in Appendix E.
- An additional suffix may be used, as follows: '1350' for (a), (b) and (c).
- The suffix 'A' has been omitted from the conductor code for (g), (h) and (i).
- 1.3 REFERENCED DOCUMENTS. The following documents are referred to in this Standard:

docume	nts are referred to in this Standard.
AS	
1391	Methods for tensile testing of metals
1442	Carbon steels and carbon-manganese steels—Hot-rolled bars and semi-finished products
1650	Galvanized coatings
1852	International electrotechnical vocabulary
2505	Methods for bend and related testing of metals
2505.5	Part 5: Torsion and wramping tests on wire
2848	Aluminium and aluminium alloys— Compositions and designations
2848.1	Part 1: Wrought products

- 2857 Timber drums for insulated electric cables and bare conductors
- C365 Drums for bare stranded conductors
- C365.II Part II: Metal drums

IEC
468 Methods of measurement of resistivity of metallic materials

ASTM

D 566 Dropping point of lubricating grease

- 1.4 **DEFINITIONS.** For the purpose of this Standard, the definitions in AS 1852 and those below apply.
- 1.4.1 Wire—A solid circular component from which stranded conductor is constructed.
- 1.4.2 King wire—a central core wire having a nominal diameter larger than that of the surrounding wires.
- 1.4.3 Conductor—a finished circular stranded conductor consisting of seven or more wires laid up together.
- 1.4.4 Diameter—the mean of two measurements at right angles taken at any one cross-section.
- **1.4.5 Direction-of-lay**—the direction of lay is defined as right-hand or left-hand, as follows:
- (a) Right-hand lay—the slope of the wires is in the direction of the central part of the letter Z when the conductor is held vertically.
- (b) Left-hand lay—the slope of the wires is in the direction of the central part of the letter S when the conductor is held vertically.
- 1.4.6 Lay ratio—the ratio of the axial length of a complete turn of the helix formed by an individual wire in a conductor, to the external diameter of the helix.
- 1.4.7 Breaking load—the maximum load obtained in a tensile test.
- 1.4.8 Ultimate tensile stress—the breaking load divided by the original cross-sectional area of the test wire.
- 1.4.9 Ungreased conductor—a conductor which is dry and free from grease, other than a light residue of wire drawing lubricant that may be on the wires.
- 1.4.10 Partly greased conductor—a conductor of more than seven wires in which grease is applied only to the steel portion.
- 1.4.11 Fully greased conductor—a conductor in which grease is applied to all wires with the exception of the outermost layer.
- 1.4.12 Surface fracture—a crack on the surface of a wire visible to an observer with normal or corrected vision.
- 1.4.13 Spool—a container of wire which is to be installed on a stranding machine to manufacture the conductor.

SECTION 2. MATERIAL REQUIREMENTS AND WIRE PROPERTIES

2.1 GENERAL The conductor shall be constructed of aluminium or aluminium alloy wires reinforced with steel wires having the properties specified herein.

The conductor may contain grease for additional protection against corrosion.

It is not intended that wires from a conductor purporting to comply with this Standard should be subjected to chemical analysis.

2.2 MATERIALS.

2.2.1 Aluminium and aluminium alloys. The aluminium and aluminium alloys shall comply with the alloy designations 1350, 1120 and 6201A, the compositions of which are specified in AS 2848.1.

2.2.2 Steel.

2.2.2.1 General. The base metal for steel reinforcing wire shall be fully-killed steel in accordance with AS 1442. The wire shall be zinc-coated (galvanized-GZ), aluminium-coated (aluminized-AZ) or aluminium-clad (AC).

2.2.2.2 Zinc-coated steel. The wire shall be zinc-coated, using either the hot dip or electrolytic process, and the coating shall comply with the relevant requirements of Clause 4.3.1. If the hot-dip galvanizing process is used, the purity of the zinc fed into the bath shall be not less than 98.5 percent. The wire before coating shall not be copper plated.

2.2.2.3 Aluminium-coated steel. The aluminium

used for aluminium coating shall conform to the following impurity limits:

Copper 0.10 % max.

Iron 0.50 % max.

The coating shall comply with the relevant requirements of Clause 4.3.2.

2.2.2.4 Aluminium-clad steel. The aluminium used for the cladding shall conform to the following impurity limits:

Copper Copper plus silicon plus iron 0.05 % max. 0.50 % max.

The coating shall comply with the relevant requirements of Clause 4.3.3.

2.2.3 Grease. Grease, used for additional corrosion protection, shall have a drop point of not less than 120 °C determined in accordance with ASTM D 566, (see Appendix F).

2.3 WIRE PROPERTIES.

2.3.1 General. Before stranding all wires shall have a round cross-section within the limits specified in Table 2.1. Tables 2.2 to 2.7 list standard wire sizes. For non-standard sizes, the wires shall meet the dimensional tolerances of Table 2.1 and have a minimum ultimate tensile stress corresponding to that of the next larger standard wire size.

Joints in wires shall comply with Clause 3.3. Joints may be made in the base rod or wire before final drawing.

TABLE 2.1
TOLERANCE ON DIAMETER OF WIRES

	Standard diameter	Tolerance of reference	on measurements, with to standard diameter
Material	mm	Mean diameter	Ovality (difference between max. and min. at same cross-section)
Aluminium and aluminium alloy	All diameters	± 1%	2%
Zinc-coated steel and aluminium-coated steel	≤2.85 >2.85	+ 3%, - 2% ± 2%	5% 4%
Aluminium-clad steel	≤2.5 >2.5	±0.04 mm ±1.5%	3% 3%

NOTE: Zinc or aluminium-coated wires, particularly those produced by the hot-dip process, contain inherent surface irregularities. To avoid unjustified rejection of wire that would be satisfactory for use, it is intended that these tolerances be used in gauging the uniform areas of the coated wire.

2.3.2 Aluminium and aluminium alloy wires.

2.3.2.1 General. The required properties of standard sizes of aluminium and aluminium alloy wires are given in Tables 2.2 to 2.4 inclusive.

Standard values adopted for the basic properties of aluminium and aluminium alloy wires for the purposes of this Standard are set out in Clauses 2.3.2.2 to 2.3.2.6.

2.3.2.2 Density. The density of aluminium and aluminium alloy wire is taken as 2700 kg/m³ at 20 °C.

2.3.2.3 Resistivity. The maximum values of resistivity at 20°C of the aluminium and aluminium alloy wires are taken to be:

Aluminium alloy 1350 0.0283 $\mu\Omega$.m Aluminium alloy 1120 0.0293 $\mu\Omega$.m Aluminium alloy 6201A 0.0328 $\mu\Omega$.m

2.3.2.4 Constant-mass temperature coefficients of resistance (α_{20}). The constant-mass temperature coefficients of resistance of aluminium and aluminium alloy wires at 20 °C, measured between two potential points rigidly fixed to the wire, are taken to be:

Aluminium 1350 0.004 03 per °C Aluminium alloy 1120 0.003 90 per °C Aluminium alloy 6201A 0.003 60 per °C

2.3.2.5 Modulus of elasticity. The modulus of elasticity of aluminium and aluminium alloy wires is taken as 68 GPa.

2.3.2.6 Coefficient of linear expansion. The coefficient of linear expansion of aluminium and aluminium alloy wires is taken as 23.0×10^{-6} per °C.

TABLE 2.2
PROPERTIES OF ALUMINIUM 1350 WIRES

1	2	3	4	5	6	7	8
•	Diameter		Cross-sectional area*	Mass per per km*	Minimum breaking load	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20 °C*
Std. mm	Max. mm	Min. , mm	mm²	kg	kN.	MPa	Ω
1.75	1.768	1.733	2.405	6.49	0.445	185	11.8
2.50	2.525	2.475	4.909	13.3	0.859	175	5.76
2.75	2.778	2.723	5.940	16.0	1.01	170	4.76
3.00	3.030	2.970	7.069	19.1	1.20	170.	4.00
3.25	3.283	3.218	8.296	22.4	- 1.37	165	3.41
3.50	3.535	3.465	9.621	26.0	1.59	165	2.94
3.75	3.788	3.713	11.04	29.8	1.77	160	2.56
4.75	4.798	4.703	17.72	47.8	2.84	160	1.60

^{*} Tabulated values are based on the standard diameters given in Column 1 and are given for information only.

TABLE 2.3
PROPERTIES OF ALUMINIUM ALLOY 1120 WIRES

1	2	3	4	5	6	7	8
	Diameter		Cross-sectional area*	Mass per km*	Minimum breaking load*	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20°C*
Std. mm	Max. mm	Min. mm	mm²	kg	k.N	MPa	Ω
2.50 2.75	2.525 2.778	2.475 2.723	4.909 5.940	13.3 16.0	1.23 1.49	250 250	5.97 4.93
3.00 3.25 3.50 3.75	3.030 3.283 3.535 3.788	2.970 3.218 3.465 3.713	7.069 8.296 9.621 11.04	19.1 22.4 26.0 29.8	1.77 2.07 2.31 2.65	250 250 240 240	4.14 3.53 3.05 2.65
4.75	4.798	4.703	17.72	47.8	4.08	230	1.65

^{*} Tabulated values are based on the standard diameter given in Column 1 and are given for information only.

2.3.3 Steel wires.

2.3.3.1 General. The required properties of standard steel wires are given in Tables 2.5, 2.6 and 2.7.

Standard values adopted for the basic properties of steel wires for the purposes of this Standard are set out in Clauses 2.3.3.2 to 2.3.3.6.

2.3.3.2 Density. The density of steel wire at 20 °C is taken to be:

Zinc-coated (GZ) 7800 kg/m³
Aluminium-coated (AZ) 7600 kg/m³
Aluminium-clad (AC) 6590 kg/m³

2.3.3.3 Resistivity. The resistivity of steel wire varies considerably with steel quality, tensile strength, and coating/cladding thickness. Maximum values at 20°C are taken to be:

Zinc-coated (GZ) 0.17 $\mu\Omega$.m Aluminium-coated (AZ) 0.15 $\mu\Omega$.m 0.085 $\mu\Omega$.m

2.3.3.4 Constant-mass temperature coefficient of resistance (α_{20}). The constant-mass temperature coefficient of resistance of steel wire at 20 °C, measured between two potential points rigidly fixed to the wire, are taken to be:

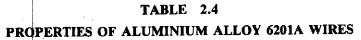
Zinc-coated (GZ) 0.0044 per °C Aluminium-coated (AZ) 0.0044 per °C Aluminium-clad (AC) 0.0036 per °C

2.3.3.5 Modulus of elasticity. The modulus of elasticity of steel wire is taken to be:

Zinc-coated (GZ) 193 GPa Aluminium-coated (AZ) 193 GPa Aluminium-clad (AC) 162 GPa

2.3.3.6 Coefficient of linear expansion. The coefficient of linear expansion is taken to be:

Zinc-coated (GZ) 11.5×10^{-6} per °C Aluminium-coated (AZ) 11.5×10^{-6} per °C 12.9×10^{-6} per °C



1	2	3	4	5	6	7	8
	Diameter	<u> </u>	Cross-sectional area*	Mass per km*	Minimum breaking load*	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20°C*
Std.	Max. mm	Min.	mm²	kg	kN	MPa	Ω
3.00 3.50 3.75	3.030 3.535 3.788	2.970 3.465 3.713	7.069 9.621 11.04	19.1 26.0 29.8	2.09 2.84 3.26	295 295 295	4.64 3.41 2.97
4.75	4.798	4.703	17.72	47.8	5.23	295	1.85

^{*} Tabulated values are based on the standard diameters given in Column 1 and are given for information only.

TABLE 2.5
PROPERTIES OF ZINC-COATED STEEL (GZ) WIRES

1	2	3	4	5	6	7	8
l	Diameter		Cross-sectional area*	Mass per km*	Minimum breaking load*	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20°C*
Std. mm	Max. mm	Min. mm	mm²	kg	kN	MPa	ů.
1.60 1.75 2.25	1.648 1.803 2.318	1,568 1,715 2,205	2.011 2.405 3.976	15.7 18.8 31.0	2.80 3.34 5.21	1390 1390 1310	85 71 43
2.50 2.75 3.00	2.575 2.833 3.060	2,450 2,695 2,940	4.909 5.940 7.069	38.3 46.3 55.1	6.43 7.78 9.26	1310 1310 1310	43 10 35 29 24
3.25 3.50 3.75	3.315 3.570 3.825	3, 185 3, 430 3, 675	8.296 9.621 11.04	64.7 75.0 86.1	10.9 12.6 14.5	1310 1310 1310	20 18 15

^{*} Tabulated values are based on the standard diameters given in Column 1 and are given for information only.

TABLE 2.6
PROPERTIES OF ALUMINIUM-COATED STEEL (AZ) WIRES

1	2	3	4	5	6	7	8
	Diameter		Cross-sectional area*	Mass per km*	Minimum breaking load*	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20 °C*
Std. mm	Max. mm	Min. mm	mm²	kg	kN	MPa	Ω
1.60 2.50 3.00	1.648 2.575 3.060	1.568 2.450 2.940	2.011 4.909 7.069	15.3 37.3 53.7	2.57 6.09 8.77	1280 1240 1240	75 31 21
3.75	3.825	3.675	11.04	83.9	12.9	1170	14

^{*} Tabulated values are based on the standard diameters given in Column 1, and are given for information only.

TABLE 2.7
PROPERTIES OF ALUMINIUM-CLAD STEEL (AC) WIRES

1	2	3	4 ,	5	6	7	8
	Diameter		Cross-sectional area*	Mass per km*	Minimum breaking load*	Minimum ultimate tensile stress	Maximum d.c. resistance per km at 20 °C*
Std.	Max.	Min. mm	mm ²	kg	kN	МРа	Ω
1.60	1.640	1.560	2.011	13.3	2.69	1340	42.3
1.75	1.790	1.710	2.405	15.8	3.22	1340	35.3
2.25	2.290	2.210	3.976	26.2	5.33	1340	21.4
2.50	2.540	2.460	4.909	32.4	6.58	1340	17.3
2.75	2.791	2.709	5.940	39.1	7.96	1340	14.3
3.00	3.045	2.955	7.069	46.6	9.47	- 1340	12.0
3.25	3.299	3.201	8.296	54.7	11.1	1340	10.2
3.50	3.553	3.448	9.621	63.4	12.6	1310	8.83
3.75	3.806	3.694	11.04	72.8	14.0	1270	7.70

^{*} Tabulated values are based on the standard diameters given in Column 1, and are given for information only.

SECTION 3. CONDUCTOR REQUIREMENTS

3.1 CONSTRUCTION.

3.1.1 General. The wire used in the construction of an aluminium or aluminium alloy conductor, steel reinforced, shall, before stranding, comply with the requirements of Section 2 of this Standard.

Conductors having more than one steel wire shall consist of a central steel wire with the other steel wires equally spaced circumferentially in the next layer.

No aluminium-coated steel wire shall be used in the outer layer of a conductor.

All wires in a conductor shall lie naturally in their correct positions. They shall tend to remain in position when the conductor is cut at any point, and shall permit restranding by hand after being forcibly unravelled.

- 3.1.2 King wire. A king wire may be included in the conductor (see Appendix F). The size of the king wire shall be five percent greater in diameter than that of the surrounding wires. This wire shall meet the mechanical and electrical properties of the other steel wires.
- 3.1.3 Grease. Additional protection against corrosion may be provided by the application of a grease (see Appendix F).
- 3.2 IDENTIFICATION OF ALUMINIUM ALLOY CONDUCTORS. Conductors manufactured to this Standard from either 1120 or 6201A alloys may be identified by means of a coloured thread, incorporated within the conductor, to signify the aluminium alloy employed. The thread shall be of durable non-hygroscopic material and coloured as follows: 1120—blue, 6201A—red (see Appendix F).

3.3 JOINTS IN WIRES OF CONDUCTORS.

- 3.3.1 General. All joints made during the stranding operation shall be in accordance with Clauses 3.3.2 and 3.3.3. They shall be free from visible defects but are not required to fulfil the mechanical requirements of unjointed wires.
- 3.3.2 Conductors containing seven wires. For

- conductors containing seven wires, the requirements for joints are as follows:
- (a) Aluminium or aluminium alloy wires. Joints in aluminium or aluminium alloy wires shall be made only by cold-pressure butt-welding. The minimum distance between any two joints in the conductor shall be 15 m.
- (b) Steel wires. There shall be no joint in any steel wire.
- 3.3.3 Conductors containing more than seven wires. For conductors containing more than seven wires, the requirements for joints are as follows:
- (a) Aluminium or aluminium alloy wires. Joints in aluminium and aluminium alloy wires shall be made by cold-pressure butt-welding or resistance butt-welding. Joints made by resistance butt-welding shall be annealed after welding over a distance of at least 200 mm on each side of the joint. The minimum distance between any two joints in the conductor shall be 15 m.
- (b) Steel wires. Joints in steel wires shall be made by resistance butt-welding and shall be protected against corrosion. The minimum distance between any two joints in the conductor shall be 15 m.

3.4 LAY.

- 3.4.1 Lay ratio. The lay ratio of the different layers shall be within the limits given in Table 3.1.
- 3.4.2 Direction of lay. In all constructions, the successive layers shall have opposite directions of lay, the outermost layer being right-handed. The wires in each layer shall be evenly and closely stranded.
- 3.5 STANDARD SIZES AND CALCULATED PROPERTIES OF CONDUCTORS. The standard sizes and calculated properties of aluminium and aluminium alloy conductors steel reinforced are given in Tables 3.2 to 3.4.

Code names by which the individual conductors may be referred to are listed in Appendix E.

TABLE 3.1
LAY RATIOS FOR ALUMINIUM AND ALUMINIUM ALLOY CONDUCTORS, STEEL REINFORCED

1	2	3	4	5	6	7	8	9	10	11	\12	13	14
Number of	wires	L	ay ratio c	f steel co	re		Lay ra	tio of alt	aminium (or alumin	ium alloj	layers	
Aluminium or	Steel	6-wire	layer	12-wie	e layer	6-wir	e layer	12-wii	e layer	18-wir	е ізуег	24-wir	e layer
aluminium alloy		Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.	Min.	Max.
3 4	4 3	12* 12*	18* 18*	-	<u>-</u>	<u>_</u>	<u>-</u> 14	<u>-</u>	=	_	_	=	_
6 18 30	7 1 7	13	28 		_ _ _	10 10	14 16	- 10 10	14 16	- - 10			<u> </u>
54 54	7 19	13 13	28 28	12		=	_	10 10	17 17	10 10	16 16	10 10	14 14

^{*} The lay ratios for 3/4 and 4/3 strandings are those for the composite conductor.

TABLE 3.2

STANDARD SIZES AND CALCULATED PROPERTIES OF STEEL-REINFORCED ALUMINIUM 1350 CONDUCTORS

13 14 15 16 Aluminium-clad steel reinforced conductor ACSR/AC/1350	s load aluminium per km area at 20°C m kn mm² at 20°C	3 10.6 30.7 0.923 7 12.7 37.1 0.763 8 15.1 44.1 0.641	4 22.3 68.9 0.410 5 32.7 109 0.259 6 64.4 155 0.182	3 91.6 224 0.126 0 106 263 0.108 0 122 305 0.0928	0 120 390 0.0726 0 139 457 0.0619 0 159 530 0.0533	0 180 608 0.0465 3 12.3 10.3 2.75 1 24.9 21.1 1.34	8 28.9 35.0 0.807 0 42.6 54.7 0.517
13 A	Approx. mass kg/km	113 137 163	254 385 636	913 1070 1240	1380 1620 1880	2150 83 171	218 340
9 10 11 12 Aluminium-coated steel reinforced conductor ACSR/AZ/1350	d.c. resistance per km at 20°C	276.0 	0.433	1 1	111	111	
11 11 11 11 11 11 11 11 11 11 11 11 11	/ Equiv. sluminium srea mm²	29.0	105	111	111	111	11
10 Im-coated si	Break. load kN	10.2	21.4 32.0	111	111	111	1 1
9 Aluminit	Approx. mass kg/km	118	265 399	111	111	 	11
8 conductor	d.c. resistance per km at 20°C	0.975 0.805 0.677	0.433 0.271 0.196	0.136 0.116 0.100	0.0758 0.0646 0.0557	0.0485 3.25 1.59	0.897
Zinc-coaled steel reinforced conductor ACSR/GZ/1350	Equiv. aluminium area mm²	29.0 35.1 41.8	65.2 105 144 ·	201 243 282	373 508 833	583 8.74 17.8	31.5
6 coated steel	Bresk. load kN	10.5 12.6 14.9	22.7 33.4 63.5	9.05 105 122	119 137 159	178 12.7 24.4	28.3
S Zinc-	Approx. mass kg/km	911 44: 17:	268 402 677	973 1140 1320	1440 1690 1960	2240 95 195	380
4	Cross- sectional area mm ²	34.36 41.58 49.48	77.31 120.4 181.6	261.5 306.9 356.0	431.2 506.0 586.9	672.0 16.84 34.36	49.48
3	Nominal overall diameter mm	7.5 8.3 9.0	11.3	21.0 22.8 24.5	27.0 29.3 31.5	33.8 5.3 7.5	9,0
2 ng and ameter	Steel	1/2.50 1/2.75 1/3.00	1/3.75 7/1.60 7/2.50	7/3.00 7/3.25 7/3.50	7/3.00 7/3.25 7/3.50	19/2.25 4/1.75 4/2.50	3/3.00
Stranding and	Aluminium 1350 mm	6/2.50 6/2.75 6/3.00	6/3.75	30/3.00 30/3.25 30/3.50	54/3.00 54/3.25 54/3.50	54/3.75 3/1.75 3/2.50	4/3.00

NOTES

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Preferred conductors are shown in bold type.

The cross-sectional area is the sum of the cross-sectional areas of the relevant individual wires.

Properties shown are calculated in accordance with the methods of Appendix A and are given for information purposes only.

Tabulated values given are based on standard diameters.

STANDARD SIZES AND CALCULATED PROPERTIES OF STEEL-REINFORCED ALUMINIUM ALLOY 1120 CONDUCTORS TABLE 3.3

-	2	3	4	\$	9	7	00	6	2	=	12	13	14	15	91
Strand	Stranding and wire diameter			Zinc	Zinc-coated steel reinford AACSR/GZ/1	d steel reinforced c	ced conductor	Aluminit	im-coated s	oated steel reinforce AACSR/AZ/1120	Aluminium-coated steel reinforced conductor	Alumin	ium-clad st AACS	clad steel reinforce AACSR/AC/1120	Aluminium-clad steel reinforced conductor AACSR/AC/1120
	Ctool	Nominal	-3006	Annrox	Break.	Equiv.	d.c. resistance	Approx.	Break.	Equiv.	d.c. resistance	Approx.	Break.	Equiv.	d.c. resistance
alloy	<u> </u>	overall	sectional	mass	load	aluminium	per km	mass	Daol	aluminium	per km at 20°C	mass.	loud	atuminium	at 20°C
1120 IDE	E	diameter	mm ²	kg/km	Z	mm ²		kg/km	ĸN	mm ²	C	kg/km	ΚN	mm ²	æ
***	H		97 97	121	2	107	00.700	170	17.9	40.3	0.700	163	18.4	42.7	0.662
0/3.00 5/3.75	1/3.58	3,5	77.31	268	27.9	63.0	0.448	265	26.5	63.0	0.448	254	27.6		0.424
6/4.75	_	14.3	120.4	405	40.7	101	0.279	<u>\$</u>	39.3	101	0.279	282	9.04	<u> </u>	707.0
	.	ļ	3	(33	3 13	164	0 173	١	1	.1	l	540	51.5	167	0.169
18/3.50		0.1	0.701	700	74.5	2	0 203	١		ŀ	ı	969	75.2	151	0.188
30/2.50	7/3.00	27.5	261.5	973	107	200	0.141	l	ł	1	ı	913	801 —	217	0.130
30.0					76	326	0010	ı	ļ	l	!	1070	127	254	0.111
30/3.25		8.7.2	200.0	11	97	55.0	0.120	1	١	1	1	1240	143	295	0.0961
8/2/2 8/2 8	7/3.50	24.5	230.0	1320	- - - - - - - - - - -	36.5	0.0784	ı	ı	1	l	1380	150	377	0.0750
		2 6			-	73	0 000	ļ	- 	1	1	1620	176	442	0.0639
45.25 473.25	7/3.25	31.5	2000	1960	16	491	0.0578	. 1	ı	ı	ı	1880	197	513	0.0552

VOTES:

1. Preferred conductors are shown in bold type.

2. The cross-sectional area is the sum of the cross-sectional areas of the relevant individual wires.

3. Properties shown are calculated in accordance with the methods of Appendix A and are given for information purposes only.

4. Tabulated values given are based on standard diameters.

STANDARD SIZES AND CALCULATED PROPERTIES OF STEEL REINFORCED ALUMINIUM ALLOY 6201A CONDUCTORS TABLE 3.4

-	7	3	4	\$	۰	7	90	6	10	11	12	13	14	15	91
Stranding and wire diameter	ig and imeter			Zinc-	Zinc-coated steel reinforcer AACSR/GZ/6201	reinforced c /GZ/6201A	d conductor	Alumini	im-coated s AACSR	oated steel reinforce AACSR/AZ/6201A	Aluminium-coated steel reinforced conductor AACSR/AZ/6201A	Alumin	ium-clad ste AACSE	Aluminium-clad steel reinforced conductor AACSR/AC/6201A	conductor
Aluminium alloy 6201A mm	Steel	Nominal overall diameter mm	Cross- sectional area mm ²	Approx. mass kg/km	Break. load kN	Equiv. aluminium area mm²	d.c. resistance per km at 20°C	Approx. mass kg/km	Break. Ioad KN	Equiv. aluminium area mm²	d.c. resistance per km at 20°C	Approx. mass kg/km	Break. load kN	Equiv. atuminium area mm²	d.c. resistance per km at 20°C
6/3.00 6/3.75 6/4.75	1/3.00	9.0	49.48 77.31 120.4	171 268 402	20.2 31.5 47.4	36.0 56.3 90.4	0.785 0.503 0.313	170 265 399	19.7 30.1 46.0	36.0 56.3 90.4	0.785 0.503 0.313	163 254 385	20.3 31.1 46.8	38.4 60.0 95.0	0.737 0.472 0.298
18/3.50 30/3.00 30/3.50	1/3.50 7/3.00 7/3.50	17.5 21.0 24.5	182.8 261.5 356.0	552 973 1320	60.8 117 158	147 179 244	0.193 0.158 0.116		111	111	111	540 913 1240	60.8 118 158	149 195 266	0.189 0.145 0.106

NOTES:

1. The cross-sectional area is the sum of the cross-sectional areas of the relevant individual wires.

2. Properties shown are calculated in accordance with the methods of Appendix A and are given for information purposes only.

3. Tabulated values given are based on standard diameters.

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SECTION 4. TESTS

4.1 SELECTION OF TEST SPECIMENS.

4.1.1 General. This Standard requires testing of component wires only. The wires shall be tested before stranding under a routine test procedure (see Clause 4.1.2).

Special tests may be carried out (see Clause 4.1.3) on specimens of wire taken from a sample of conductor (see Appendix F).

4.1.2 Routine tests. Routine tests shall be conducted on a specimen taken from every tenth spool of wire prepared for loading on a stranding machine and shall be tested as specified in Table 4.1.

If a sample fails a test, that test shall be repeated on two further specimens taken from the same spool. If either of these fail, the spool shall be rejected and five spools produced sequentially, before and after the rejected spool shall be individually tested.

4.1.3 Special tests. Special tests shall be conducted on wire specimens taken from a sample length of conductor from either one drum in every 200 km of conductor produced, or from one drum from every production run, whichever rate provides the largest number of samples.

Specimens shall be tested as specified in Table 4.2.

If a specimen fails a test, that test shall be repeated on a further sample of conductor taken from the same drum. If any of the wire specimens fail the retest, the drum shall be rejected, and the drum of conductor produced immediately before and the drum of conductor produced immediately after the rejected drum shall be individually tested.

4.2 MECHANICAL TESTS.

4.2.1 Dimensions. The diameter of the wire shall be measured and recorded and shall be within the limits specified in Clause 2.3.1, and where applicable in Tables 2.2 to 2.7.

4.2.2 Ultimate tensile stress test. The breaking load of each specimen, selected in accordance with Clause 4.1 shall be determined in accordance with the method given in AS 1391. The ultimate tensile stress shall be calculated on the basis of the actual cross-sectional area of the wire before testing.

For routine tests the ultimate tensile stress of the specimen shall be not less than the appropriate value given in Tables 2.2 to 2.7 inclusive.

For special tests, the ultimate tensile stress of the specimen shall be not less than 95 percent of the appropriate value given in Tables 2.2 to 2.7 inclusive.

The test specimen shall be free from bends or kinks other than the curvature resulting from the usual spooling or stranding operation.

4.2.3 Ultimate elongation test. Where specified in Tables 4.1 and 4.2, the ultimate elongation shall be determined by suitably measuring the increase in distance between the gauge marks, after carefully fitting the broken ends of the test specimen together, in accordance with the method given in AS 1391.

The elongation on a gauge length of 250 mm shall be not less than the appropriate values given in Table 4.3.

4.2.4 Torsion test. The torsion test shall be carried out in accordance with AS 2505.5 except as modified herein. The specimens of wire selected in accordance with Clause 4.1 shall each be gripped at the ends in two vices, one of which shall be free to move longitudinally during the test. A small tensile force, not exceeding 2 percent of the breaking load of the wire, may be applied to the sample during testing. The specimen shall be twisted by causing one of the vices to revolve until breakage occurs and the number of twists shall be indicated by a counter or other suitable device. The rate of twisting shall not exceed 60 turns per minute.

The number of complete twists before breakage occurs shall be not less than the values given in Table 4.4.

TABLE 4.1
SCHEDULE OF ROUTINE TESTS

Test	Clause reference	Aluminium 1350	Aluminium alloy 1120	Aluminium alloy 6201A	Zinc-coated steel	Aluminium- coated steel	Aluminium-clad steel
Dimensions Ultimate tensile stress Ultimate elongation Torsion Wrapping Coating Resistivity	4.2.1 4.2.2 4.2.3 4.2.4 4.2.5 4.3 4.4	100 100 P10 N/A 10 N/A 10	100 100 P10 N/A 10 N/A 10	100 100 P10 N/A 10 N/A 10	100 100 A A 10 10 N/A	100 100 A A 10 10 N/A	100 100 A A N/A 10

LEGEND:

= Tests to be conducted on 100% of specimens selected in accordance with Clause 4.1.2.

= Tests to be conducted on not less than 10% of specimens selected in accordance with Clause 4.1.2.

A = Ultimate elongation or torsion tests as alternative tests, to be conducted on not less than 10% of specimens selected in accordance with Clause 4.1.2.

P10 = Optional tests to be carried out on not less than 10% of specimens selected in accordance with Clause 4.1.2

N/A = Not applicable.



TABLE 4.2 SCHEDULE OF SPECIAL TESTS

Test	Clause reference	Alum 13		Aluminium alloy 1120	Aluminium alloy 6201A	Zinc-coated steel	Aluminium- coated steel	Aluminium-clad steel
Dimensions Ultimate tensile stress Ultimate elongation Torsion Wrapping Coating Resistivity	4.2.1 4.2.2 4.2.3 4.2.4 4.2.5 4.3 4.4	10 10 N/ N/ 10 N/	0 A A O A	100 100 N/A N/A 10 N/A 10	100 100 N/A N/A 10 N/A 10	100 100 A A 10 10 N/A	100 100 A A 10 10	100 100 A A N/A 10

LEGEND:

100

10

 Tests to be conducted on 100% of specimens selected in accordance with Clause 4.1.3.
 Tests to be conducted on not less than 10% of specimens selected in accordance with Clause 4.1.3.
 Ultimate elongation or torsion tests as alternative tests, to be conducted on not less than 10% of specimens selected in accordance with Clause 4.1.3. Α

N/A = Not applicable.

TABLE 4.3 **ULTIMATE ELONGATION OF WIRES**

•	Minimum ultimate p	ercentage elongation in 2	250 mm, for wires of spo	ecified diameter range
Material	>1.5 ≤ 2.50 mm	>2.50 ≤3.25 mm	>3.25 ≤4.00 mm	>4.00 ≤4.75 mm
Aluminium 1350	0.8	1.0	1.2	1.4
Aluminium alloy 1120		1.0	1.2	1.4
Aluminimum alloy 6201A		3.0	3.0	3.0
Zinc-coated steel (GZ)* Aluminium-coated steel (AZ) Aluminium-clad steel (AC)	3.0	3.5	4.0	4.0
	3.0	3.5	4.0	4.0
	1.0	1.0	1.3	1.5

Elongation tests are not appropriate for wires drawn after zinc coating.

TABLE 4.4 MINIMUM TORSION REQUIREMENT FOR STEEL WIRES

	Oi	Minimum number of n a length of 100 time	twists to breakage is the wire diameter
Wire condition	Zinc- coated (GZ)	Aluminium- coated (AZ)	Aluminium-clad (AC)
Before stranding After stranding	18 16	18 16	20 20

NOTE: The test length may be varied from 100 times the wire diameter, in which case the number of twists to breakage shall be adjusted pro rata. The calculated number of twists to breakage shall be a whole number, with fractions of a twist to be taken as one twist.

4.2.5 Wrapping test. The wrapping test shall be carried out in accordance with AS 2505.5 except as modified herein. The specimens of wire selected in accordance with Clause 4.1 shall each be wrapped around a wire of its own diameter to form a close helix of eight turns. The wrapping rate shall not exceed 60 turns per minute. Where applicable the specimens shall be unwrapped and rewrapped, according to the schedule specified in Table 4.5. The wire shall meet the acceptance criteria of Table 4.5.

TABLE 4.5
WRAPPING TEST REQUIREMENTS

Material			edule f turns	Acceptance
.,	On	Of	On	criterion
Zinc-coated steel (GZ) Aluminium-coated steel	8	7	-	Shall not break
(AZ)	. 8	7		Shall not break
		:	N/A	
Aluminium 1350	8	6	6	Shall not break
Aluminium alloy 1120	8	_		No surface fracture
Aluminium alloy 6201A	8	_	-	No surface fracture

N/A = Not applicable.

4.3 COATING TESTS.

4.3.1 Zinc-coated wire. Coating tests shall be made on specimens of wire selected in accordance with Clause 4.1.

The mass, quality and adherence of the zinc coating whether applied by the hot dip or the electrolytic process shall be tested in accordance with AS 1650. The mass of coating shall be not less than that specified in Table 4.6.

TABLE 4.6

MASS OF ZINC COATING FOR STEEL WIRES

Nominal diamete	er of coated wire	Minimum coating mass
m	m	g/m ²
≥ 1.55	≤ 1.80	200
> 1.80	≤ 2.24	215
> 2.24	≤ 2.72	230
> 2.72	≤ 3.15	240
> 3.15	≤ 3.55	250
> 3.55	≤ 4.25	260

4.3.2 Aluminium-coated wire.

4.3.2.1 General. Coating tests as prescribed in Clauses 4.3.2.2 to 4.3.2.4 shall be made on specimens of wire selected in accordance with Clause 4.1.

4.3.2.2 Adherence of coating. The wire shall be capable of being wrapped in a close helix at a rate not exceeding 15 turns per minute around a cylindrical steel mandrel having a diameter as prescribed in Table 4.7, without cracking or flaking the aluminium coating.

NOTE: Loosening or detachment during the adherence test of superficial small particles of aluminium formed by mechanical polishing of the surface of aluminium coated wire is not considered cause for rejection.

TABLE 4.7

MANDREL SIZE FOR ADHERENCE TEST FOR ALUMINIUM-COATED WIRES

Standard diameter of aluminium-coated wire mm	Ratio of mandrel diameter to wire diameter
≥1.60 ≤2.25 >2.25 ≤3.50	3 4
>3.50	

4.3.2.3 Continuity of coating. Testing wire for continuity of the aluminium coating may be carried out using the method given in Appendix C (see Appendix F).

4.3.2.4 Mass of coating. The mass of aluminium coating on the steel wire shall be determined by the method described in Appendix D and shall conform with the values given in Table 4.8.

TABLE 4.8

MINIMUM MASS OF ALUMINIUM COATING
FOR STEEL WIRES*

Wire diameter mm	Minimum mass of aluminium coating g/m ²
1.60	77
. 2.25	80
2.50	86
3.00	92
3.50	98
3.75	104
3.75	104

* Wire with diameter intermediate to those shown shall have a coating mass equal to the next larger size.

4.3.3 Aluminium-clad wire. Measurement of the radial thickness of the aluminium cladding shall be made on each of the specimens of aluminium-clad wire selected in accordance with Clause 4.1.

Measurement to an accuracy of 0.02 mm shall be made by cutting off suitable specimens, preparing and etching the cross-section and measuring with an optical instrument or by using a suitable indicating instrument.

The radial thickness of aluminium cladding at any point on the wire shall be not less than five percent of the standard diameter of the aluminium-clad steel wire

4.4 RESISTIVITY TEST. The specimens of aluminium, aluminium alloy and aluminium-clad steel wire selected in accordance with Clause 4.1 shall each be measured for electrical resistance in accordance with the method given in IEC 468 to an accuracy of at least one part in a thousand at a temperature of not less than 10°C nor more than 30°C. The length of the specimen shall be sufficient to give the accuracy required and shall be suitable for the method of testing used.

The value of resistance, measured at a temperature of $T(^{\circ}C)$, shall be corrected to that at $20^{\circ}C$, by multiplying the measured value by a correction factor (K), given by:

$$K = \frac{1}{1 + \alpha_{20} (T - 20)}$$

where

 α_{20} is the appropriate constant mass temperature coefficient of resistance, as per Clauses 2.3.2.4 and 2.3.3.4.

The resistivity shall be calculated from the corrected resistance, and its value shall not exceed the values given in Clause 2.3.2.3 or Clause 2.3.3.3, as appropriate.

4.5 LAY RATIO. The lay ratios shall be checked and recorded at the beginning and end of each production run of any one size of conductor, by measuring the lays with the conductor under tension on the stranding machine.

The lay ratios shall be within the appropriate limits specified in Table 3.1.

- **4.6 PLACE OF TESTING.** All tests shall be made at the manufacturer's works.
- 4.7 INSPECTION. Inspection shall be made at the manufacturer's works.
- 4.8 TEST CERTIFICATE. The manufacturer shall supply the purchaser with either a certificate giving the results of tests made on the specimens selected in accordance with Clause 4.1, or a written statement that the conductor complies with this Standard.

SECTION 5. PACKING AND MARKING

- 5.1 PACKING. The conductor shall be supplied on drums constructed to the requirements of AS 2857 or AS C365, Part II.
- 5.2 MARKING. The following information shall be legibly and durably marked on the flange of the drum or on a label:
- (a) Manufacturer's name.
- (b) Manufacturer's drum serial number.
- (c) Size and type of conductor.
- (d) Whether conductor is ungreased, partially greased or wholly greased.
- (e) Length of conductor.
- (f) Gross mass of drum and conductor.
- (g) Handling or lifting instructions where such handling or lifting is by means other than a spindle through the spindle holes with spreader to prevent damage to flanges.
- (h) An arrow with the words 'ROLL THIS WAY' to indicate the direction in which the drum should be rolled on the flanges.

NOTES:

- An acceptable means of marking all or part of the above information would be a waterproof plate or label securely attached to the drum (see Appendix F).
- Manufacturers making a statement of compliance with this Australian Standard on a product, or on packaging or promotional material related to that product, are advised to ensure that such compliance is capable of being verified.

Independent certification is available from Standards Australia under the StandardsMark Product Certification Scheme. The StandardsMark, shown below, is a (registered) certification trade mark owned by Standards Australia and granted under licence to manufacturers whose products comply with the requirements of suitable Australian Standards and who operate sound quality assurance programs to ensure consistent product quality.

Further information on product certification and the suitability of this Standard for certification is available from Standards Australia's Quality Assurance Services, 80 Arthur Street, North Sydney, N.S.W., 2060.

APPENDIX A

CALCULATION OF CONDUCTOR PROPERTIES

(This Appendix does not form an integral part of this Standard.)

- A1 GENERAL. The values given in Tables 3.2 to 3.4 inclusive and in this Appendix are based on standard diameters and are given for information purposes only. Tests for these properties do not form part of the requirements of this Standard.
- A2 INCREASE IN LENGTH DUE TO STRANDING. When straightened, each wire in any particular layer of a conductor, except the central wire, is longer than the conductor by an amount depending on the mean lay ratio of that layer as derived from Table 3.1.

NOTE: The mean lay ratio is the arithmetic mean of the relevant maximum and minimum values given in Table 3.1.

A3 MASS OF CONDUCTOR. The mass of each wire in a length of conductor, except the central wire, will be greater than that of an equal length of straight wire by an amount depending on the mean lay ratio of the layer as derived from Table 3.1. The total mass of an aluminium or aluminium alloy conductor, steel reinforced, is obtained by calculating the mass of the aluminium or aluminium alloy and steel wires separately, and adding them together. The mass of each component material is obtained by multiplying the mass of an equal length of straight wire by its respective mass constant set out in Table A1.

A4 DIRECT CURRENT RESISTANCE OF CONDUCTOR.

- A4.1 General. The resistance of any length of a conductor is obtained by multiplying the resistance of an equal length of straight wire by its respective resistance constant set out in Table A1.
- A4.2 Resistance, conductor types: (ACSR/GZ), (AACSR/GZ). For conductor of 3/4 and 4/3 construction, because of the high proportion of steel in the conductor, the resistance is calculated as in Clause A4.4.

For other conductors, the resistance is calculated with reference to the resistance of the aluminium or aluminium alloy wires only. The conductivity of the zinc-coated steel wire(s) is not taken into account.

- A4.3 Resistance, conductor types: (ACSR/AZ), (AACSR/AZ). The resistance of the conductor is calculated with reference to the aluminium or aluminium alloy wires only. The conductivity of the aluminium coated steel wire(s) is not taken into account.
- A4.4 Resistance, conductor types: (ACSR/AC), (AACSR/AC). The resistance of the conductor is obtained by taking the resistance of the aluminium or aluminium alloy wires, and the aluminium-clad steel separately. The parallel equivalent resistance of the two components is then calculated.

A5 EQUIVALENT ALUMINIUM AREA.

- A5.1 General. The term 'equivalent aluminium area' denotes the area of a solid aluminium 1350 rod which would have the same resistance as the conductor. This area takes into account the assumed increase of resistance of each wire except the central wire (see Paragraph A2 above), and any differences in resistivity between the component materials of the conductor and aluminium 1350. The equivalent aluminium area of a conductor is the sum of the areas of the appropriate component wires.
- A5.2 Aluminium and aluminium alloy. The equivalent aluminium area of the aluminium or aluminium alloy is obtained by multiplying the area of one wire by—
- (a) the appropriate area constant set out in Table A1; and in the case of aluminium alloy wires by—
- (b) the ratio of the resistivity of aluminium 1350 to that of the aluminium alloy (see Clause 2.3.2.3).
- A5.3 Zinc-coated steel. The equivalent aluminium area of the zinc-coated steel is taken into account only for conductors of 3/4 and 4/3 construction (see Paragraph A4 above).
- A5.4 Aluminium-coated steel. The equivalent aluminium area of the aluminium-coated steel is not taken into account.

- A5.5 Aluminium-clad steel. The equivalent aluminium area of the aluminium-clad steel is obtained by multiplying the area of one wire by both—
- (a) the appropriate area constant set out in Table A1; and
- (b) the ratio of the resistivity of aluminium 1350 to the resistivity of aluminiumclad steel (see Clause 2.3.3.3).
- A6 CALCULATED BREAKING LOAD OF CONDUCTOR. The calculated breaking load of an aluminium or aluminium alloy conductor, steel reinforced, (in terms of the sum of the strengths of the individual component wires before stranding), is taken as 98 percent of the sum of the strengths of the aluminium or aluminium alloy wires plus 85 percent of the sum of the strengths of the steel wires based on the calculated minimum breaking loads of the component wires.

NOTE: The actual breaking load may vary from the calculated value by 5 percent.

TABLE A1
STRANDING CONSTANTS, AREA, MASS AND RESISTANCE

1	2	3	4	5	6	7	8	9
Number of w	ires	Are	a and mass s	tranding con	stants	Resis	tance stranding c	onstants
in conducto			nium or ium alloy	St	eel	Aluminium or	Galvanized	Aluminium- clad
Aluminium or aluminium alloy	Steel	Area	Mass	Area	Mass	aluminium alloy	steel	steel
3 4 6	4 3 1	2.971 3.962 5.910	3.029 4.039 6.091	3.971 2.981 1.000*	4.029 3.019 1.000	0.3366 0.2524 0.1692	0.2518 0.3355 —	0.2518 0.3355 1.000
6 18 30	7 1 7	5.910 17.67 29.34	6.091 18.34 30.67	6.968* 1.000* 6,968*	7.032 1.000 7.032	0.1692 0.05660 0.03408	<u>-</u> .	0.1435 1.000 0.1435
.54 .54	7 19	52.80 52.80	55.23 55.23	6.968* ; 18.85*	7.032 19.15	0.01894 0.01894	=	0.1435 0.5305

^{*} Applicable only to aluminium-clad steel.

APPENDIX B

CALCULATION OF MODULUS OF ELASTICITY AND COEFFICIENT OF LINEAR EXPANSION

(This Appendix does not form an integral part of this Standard.)

B1 MODULUS OF ELASTICITY.

B1.1 General. The final modulus of elasticity of a non-homogeneous conductor is dependent on a number of factors including the conductor's previous thermal and tensile history, the method of stranding and the actual conductor configuration. Theoretical values of the modulus can however be calculated from a knowledge of the component material properties and assuming a specific conductor construction. The calculation takes into account the fact that only the centre wire lies parallel to the conductor's axis.

B1.2 Calculation. The calculated values of the final modulus given in Table B1 have been determined using the method of Nigol and Barrett* and the following assumptions:

- (a) The mean lay ratio has been used (see Paragraph A2).
- (b) No slippage between steel core and aluminium or aluminium alloy wires.
- (c) No radial elastic component.
- (d) Material moduli in accordance with Clauses 2.3.2.5 and 2.3.3.5. The following relationships apply*:

$$\tan \theta_{i} = \frac{2\pi r_{i}}{L_{i}D_{i}}$$

$$E_{ij} = Ew_{ij} \cos^{3}\theta_{i}$$

$$E_{f} = \frac{1}{A_{T}} \left\{ E_{c}A_{c} + \sum_{j=1}^{N_{i}} \left[\sum_{i=1}^{n} \left(m_{ij}A_{ij}E_{ij} \right) \right] \right\}$$

where

 L_i = mean lay ratio of layer i

 D_i = external diameter of layer i

 r_i = radius of layer i, from centre of conductor to centre of wire in the layer

 θ_i = lay angle of wires in layer i

 Ew_{ii} = material modulus of wires in layer i of material j

 E_{ij} = wire modulus in layer *i* of material *j*

 m_{ij} = number of wires in layer i of material j

 N_i = number of materials in layer i

n = number of layers

 E_c = central wire material modulus

 $E_{\rm f}$ = calculated final non-homogeneous conductor modulus

 A_{ij} = area ϕf wire in layer i of material j

 A_c = area of central wire

 $A_{\rm T}$ = total cross-sectional area of conductor

B2 COEFFICIENT OF LINEAR EXPANSION.

B2.1 General. The coefficient of linear expansion (CLE) of a non-homogeneous conductor may be calculated from a knowledge of the material properties and the areas of each component making up the conductor.

^{*} The method used to determine the modulus of elasticity was derived from a report prepared for the Canadian Electrical Association under Contract 78-93, March 1982, titled Development of an Accurate Model of ACSR Conductors for Calculating Sags at High Temperature—Part 3, by D. Nigol and S. Barrett.

- **B2.2 Calculation.** The values of the coefficient of linear expansion in Table B1 have been determined assuming there is no slippage between steel and aluminium and using the following material properties:
- (a) Material moduli is in accordance with Clauses 2.3.2.5 and 2.3.3.5.
- (b) Material coefficient of linear expansion is in accordance with Clauses 2.3.2.6 and 2.3.3.6.

The following relationship applies:

$$\alpha_{\rm c} = \frac{A_1 E_1 \alpha_1 + A_2 E_2 \alpha_2}{A_1 E_1 + A_2 E_2}$$

where

 A_1, A_2 = area of material 1, 2

 E_1 , E_2 |= modulus of material 1, 2

 $\alpha_1, \alpha_2 = CLE \text{ of material } 1, 2$

= CLE of non-homogeneous conductor

TABLE B1
MODULUS OF ELASTICITY AND COEFFICIENT OF LINEAR EXPANSION

Number of wi	res	Fi	nal modulus o	f electricity, GP	я	Calculated coef	
Aluminium or aluminium alloy	Steel	ACSR/GZ AACSR/G		ACSI AACS		per degree Co	elsius
		Calculated	Practical	Calculated	Practical	ACSR/GZ and AZ AACSR/GZ and AZ	ACSR/AC AACSR/AC
6 6 18	1 7 1	83 80 71	<u>-</u>	79 76 69		19.3 × 10 ⁻⁶ 19.9 × 10 ⁻⁶ 21.4 × 10 ⁻⁶	$\begin{array}{c} 20.1 \times 10^{-6} \\ 20.6 \times 10^{-6} \\ 21.8 \times 10^{-6} \end{array}$
30 54 54	7 7 19	88 78 77	81-85 74 69-73	82 75 74	78-80 — —	$ \begin{array}{r} 18.4 \times 10^{-6} \\ 19.9 \times 10^{-6} \\ 20.0 \times 10^{-6} \end{array} $	$\begin{array}{c} 19.4 \times 10^{-6} \\ 20.6 \times 10^{-6} \\ 20.7 \times 10^{-6} \end{array}$
3 4	4 3	136 119	_	119 106	<u>-</u>	13.9 × 10 ⁻⁶ 15.2 × 10 ⁻⁶	15.3×10^{-6} 16.5×10^{-6}

NOTES:

- Practical values of conductor modulus based on actual conductor test measurements have been provided where available. The calculated values are regarded as being of sufficient accuracy for direct use in conductor sag/tension calculations.
- 2. Coefficient of linear expansion values quoted may be taken as applying to conductors with a maximum operating temperature of 100 °C.
- 3. Tabulated values given are based on standard diameters and are given for information only.

APPENDIX C

A CONTINUITY OF COATING TEST FOR ALUMINIUM-COATED STEEL

(This Appendix does not form an integral part of this Standard.)

- C1 SCOPE. A suitable test which has been applied to aluminium-coated wire in the laboratory is set put in this Appendix.
- C2 PREPARATION OF SPECIMENS. Specimens of degreased aluminium-coated steel wire are sealed at the cut ends with wax or any other suitable material.
- Prepared specimens are immersed in a solution of 1.0 percent C3 PROCEDURE. potassium ferricyanide and 0.5 percent of 98 percent sulphuric acid, in water, at an ambient temperature of 20 ±3 °C.
- C4 RESULTS. Pinholes and other discontinuities in the coating are indicated by the formation of dark blue spots.

Any pinholes which do not appear within five minutes may be considered insignificant.

- This test depends on the formation of ferrous sulphate by the action of the sulphuric acid on the
 exposed iron, followed by a reaction between the ferrous sulphate and the potassium ferricyanide
 to form potassium ferric ferrocyanide (prussian blue).
- 2. Care should be taken to avoid agitation of the solution during the test as the prussian blue formed will mix with the body of the solution and not be localized at the pinholes. This may also happen by diffusion if the test is prolonged.
- 3. Potassium ferricyariide should not be confused with potassium cyanide, which is extremely toxic. Normal methods of handling chemicals are recommended.
- 4. It is considered that occasional small pinholes in the coating would not have a serious effect on the suitability of the wire for service. Aluminium is normally anodic to iron in the electrolytic cell set up under corrosive conditions and would be expected to corrode preferentially. Also, the large area of aluminium (anode) to iron (cathode) would also be expected to inhibit the corrosion of the iron.

APPENDIX D

DETERMINATION OF MASS OF ALUMINIUM COATING

(This Appendix forms an integral part of the Standard.)

D1 SCOPE. This Appendix sets out the method for determining the mass of aluminium coating on wire.

D2 PREPARATION OF SPECIMENS. The specimens of wire shall be selected in accordance with Clause 4.1.2 or Clause 4.1.3.

The specimens to be stripped may be any length, but preferably over 300 mm. It is not necessary to measure the length. The specimen may be cut into convenient lengths (about 150 mm), for the determination of mass on a chemical balance; the several pieces may be dealt with as one specimen for the determination of mass and the stripping.

The specimens shall be cleaned by washing in petroleum ether or other suitable solvent and dried thoroughly, immediately before the determination of mass.

- D3 REAGENTS. The following reagents shall be used:
- (a) Sodium hydroxide solution (20 percent). Dissolve 20 parts by mass of sodium hydroxide (NaOH) in 80 parts of water.
- (b) Hydrochloric acid ($\varrho = 1190 \text{ kg/m}^3$).

- D4 PROCEDURE. The procedure shall be as follows:
- (a) Before stripping, determine the mass of the specimens. The determination of mass may be carried out on individual specimens, or on a number of specimens together depending on whether a minimum or average value of the mass of coatings is desired.
- (b) Heat the sodium hydroxide solution to between 90 °C and 100 °C (Note 1) and immerse each specimen in the hot solution until the strong reaction ceases. With silicon-free coatings, gas may be evolved for a considerable time but the specimens should not be left in the solution for more than a few minutes. Longer immersion inhibits the removal of coating during subsequent dips. Several specimens may be immersed simultaneously provided all surfaces are freely exposed to the solution.
- (c) Remove the specimens and wipe with a clean cellulose sponge under running water to remove the loose deposit formed in the hot solution. Blot with a towel to remove most of the water (Note 2) and immerse each specimen singly for not more than 3 s in hydrochloric acid at room temperature. Remove, clean again with a sponge under water, and re-immerse in the hot solution for not more than a few minutes or until action again ceases. Repeat cycle until immersion in hydrochloric acid shows no visible reaction (Note 3). One to three or more cycles may be required, depending on the type of coating.
- (d) After the final immersion in the sodium hydroxide and hydrochloric acid solutions, clean as before and dry thoroughly. Determine the mass and diameter of the wire after stripping. The diameter should be measured to the nearest 0.01 mm by taking the average of two measurements made at right angles to each other.

D5 CALCULATION. Calculate the mass of aluminium coating in grams per square metre as follows:

Mass of coating =
$$\frac{m_1 - m_2}{m_2} \times D \times 1960$$

 m_1 = original mass of specimen, in grams

 m_2 = mass of stripped specimen, in grams

D = diameter of stripped specimen, in millimetres.

D6 REPORT.NOTES:
The mass of coating shall be reported to the nearest whole number.

- The temperature is not critical but the solution should be held several degrees below the boiling point
 (approximately 105°C) to prevent excessive foaming during the first immersion. The beaker used for heating
 the solution and immersing the specimens should be less than half full of solution to avoid the danger
 of foaming over when the specimens are immersed.
- Most of the water should be removed to prevent dilution of the hydrochloric acid. (Dilute hydrochloric acid will attack the base metal to a greater extent than concentrated acid.)
- 3. It is sometimes difficult to determine the point at which all the aluminium layer has been removed when stripping silicon-free coatings. If in doubt, determine the mass of the specimen (after scrubbing and drying) and then put the specimen through one additional stripping cycle. Loss in mass due to the additional cycle will be of the order of 0.75 g/m² if all the coating has been removed before the extra cycle.

APPENDIX E

CODE NAMES FOR ALUMINIUM AND ALUMINIUM ALLOY CONDUCTORS, STEEL REINFORCED

(This Apperdix does not form an integral part of the Standard.)

Table E1 gives code names for aluminium conductors steel reinforced.

For aluminium alloy conductors steel reinforced, code names are given by the code for the corresponding stranding of aluminium conductor steel reinforced, together with a suffix indicating the alloy type.

Lemon 1120.

e.g. 30/7/3.00 ACSR/GZ: 30/7/3.00 AACSR/GZ/1120: 30/7/3.00 AACSR/GZ/6201:

Lemon 6201.

TABLE E1 CODE NAMES FOR ALUMINIUM CONDUCTORS STEEL-REINFORCED

tranding and wire di	ameter, mm	Zinc-coated steel reinforced	Aluminium-coated steel reinforced	Aluminium-clad steel reinforced
Aluminium	Steel	ACSR/GZ	ACSR/AZ	ACSR/AC
6/2.50	1/2.50	Almond	Barley	Angling
6/2.75	1/2.75	Apricot	-	Aquatics
6/3.00	1/3.00	Apple	Bean	Archery
6/3.75	1/3.75	Banana	Cabbage	Baseball
6/4.75	7/1.60	Cherry	Carrot	Bowls
18/3.50	1/3.50	Fig		Boxing
30/2.50	7/2.50	Grape		Cricket
30/3.00	7/3.00	Lemon	l <u> </u>	Darts
30/3.25	7/3.25	Lychee		Dice
30/3.50	7/3.50	Lime	_ `	Diving
54/3.00	7/3.00	Mango		Golf
54/3.25	7/3.25	Orange		Gymnastics
54/3.50	7/3.50	Olive	_	Hurdles
54/3.75	19/2.25	Pawpaw	_	Lacrosse
3/1.75	4/1.75	Ouince		Skating
3/1./3 3/2.50	4/2.50	Raisin		Soccer
4/3.00	3/3.00	Sultana	<u></u>	Swimming
4/3.75	3/3.75	Walnut	1 - 1	Tennis ·

NOTE: Sizes shown in bold type are preferred sizes for ACSR conductors 18/3.50 - 1/3.50 size is a preferred size for AACSR/1120 only.

APPENDIX F

ITEMS TO BE SPECIFIED BY THE PURCHASER OR SUBJECT TO AGREEMENT BETWEEN THE PURCHASER AND MANUFACTURER

(This Appendix does not form an integral part of the Standard.)

F1 GENERAL. Some of the items listed are additional to the purchasing details normally provided by the purchaser at the time of order and should either be specified by the purchaser or be subject to agreement between the purchaser and manufacturer.

F2 ITEMS TO BE SPECIFIED BY THE PURCHASER.

والأفائد المساد السيادا الأرادا فالمستقر الرشيون الراري

- (a) Whether the conductor is to be greased and if so wholly or partly, and whether the grease must have other special characteristics, (see Clause 2.2.3 and Clause 3.1.3).
- (b) Whether a king wire is required, (see Clause 3.1.2).
- (c) Requirement for coloured thread identifiers, for alloy 1120, and alloy 6201A, (see Clause 3.2).
- (d) Whether special tests are required (see Clause 4.1.1).
- (e) Whether optional routine tests (P10) are to be carried out (see Table 4.1).
- (f) Whether a continuity of coating test is required for aluminium coated (AZ) wire, and if so, the method to be used, (see Clause 4.4.2.3).
- (g) Requirements for test certificates, (see Clause 4.8).
- (h) Requirements for any additional information to be marked on the drum flange or the label, see Clause 5.2, and any special method of marking if not in accordance with Note 1 of Clause 5.2.